

ISO 3297:2007 Certified Vol. 3, Issue 7, July 2016

# Modelling of turning process for Prediction of tool wear

Bhagyashri D. Deore<sup>1</sup>, Dr. P.S. Desale<sup>2</sup>

PG Student, Mechanical Department, S.S.V.P.S.B.S. Deore College of Engineering, Dhule, India <sup>1</sup> Associate Professor, Mechanical Department, S.S.V.P.S.B.S. Deore College of Engineering, Dhule, India <sup>2</sup>

**Abstract**: The tool wear is measured by using a Profile Projector PP-200. In this indirect measurement technique the tools wear parameters are cutting speed, feed and depth of cut. In addition to that software computer techniques adaptive neuro-fuzzy inference system is applied for Modelling prediction. The objective of this study is also to correlate flank wear in regression and compare with ANFIS in prediction studies. The proposed model is for prediction of flank wear of the mild steel work piece. The machining experiments are performed under various cutting conditions using Cutting speed, Feed and Depth of Cut. The flank wear is measured. It is also observed that the flank wear prediction accuracy of Adaptive neuro fuzzy inference system using trapezoidal membership function is better than regression analysis. The flank wear prediction accuracy with ANFIS is 87.87% as input parameters are cutting speed, feed and depth of cut.

Keywords: Turning, ANFIS, Regression, Flank Wear, Crater Wear.

#### I. INTRODUCTION

In any manufacturing process, numbers of operations are studies is being considered for obtaining higher levels of done with the lathe machine they are turning, facing, knurling, grooving, parting, chamfering, taper turning, drilling and threading. Turning is the most important process in an industry which is done with a lathe machine. In turning process, turning is used to remove the excess material. In this operation work piece is having a rotary motion. But there are more important things in this operation such as tool life, tool wear and tool machinability. If we discuss about tool life cutting life of tool is expressed in time. Time period measured from start of cut of failure of the tool. Wear is progressive damage, involving material loss, occurs on the surface as a result of relative motion between the surfaces. Tool wear causes the tool to lose its original shape- ineffective cutting, Tool needs to be resharpened. There is a geometry of tool wear they are flank wear (edge wear) and crater wear (face wear).

In flank wear, tool slides over the surface of the work piece and friction is developed. It occurs due to friction and abrasion. Adhesion between work piece & tool- BUE. It starts at CE and starts widening along the clearance face. In flank wear, independent of cutting conditions and tool / work piece materials, brittle and discontinuous chip. It increases as speed is increased. The work reported for turning process by acoustic emission technique and artificial intelligence technique correlative to flank wear analysis of single point turning. (et al. 2008) is that the experimental results obtained on measurement and the trained network generated attributes correlate for one complete experiment. Higher degree of accuracy may be achieved when the training of network is taken up with D. Dinakaran a, S. Sampathkumar b, J. Susai Mary (et al. more number of trials and use of larger number of epochs. More than one method of wear analysis and correlatives

accuracy and for optimization.

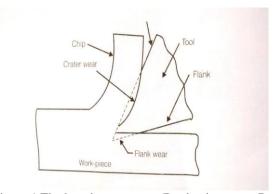


Figure 1 Flank and crater wear (Production engg. By Panday and Singh)

Heyao Shen, Minghong Wang was doing the work on the topic the simulation analysis of tool flank wear based on cutting force. They focuses on researching relationship between cutting force and tool flank wear. In different experiment conditions, the consistency of the results of simulation and experiment results was obtained through the comparative analysis between the two. It is mainly investigated into the simulation analysis of the tool flank wear. The specific content of the simulation experiment is explaining the causation for the tool flank wear through the analysis of the temperature field at the tip and obtaining the data of cutting force in different tool flank wear (10,100,200,300um).

2010) used the nuero fuzzy technique in turning for the real time prediction of flank wear. An ultrasonic technique

ISO 3297:2007 Certified Vol. 3, Issue 7, July 2016

waves are reflected from wear area. They were used parameters are cutting speed, feed and depth of cut for adaptive neuro fuzzy inference system (ANFIS) for the experimentation and prediction work. tool wear. The experimental validation shows that ANFIS can predict the tool wear with average error of 2.5%.

S.Thamizhmanii\* and S.Hasan (et al. 2010) wear discussed about CBN and PCBN tools due to cutting Experimental set up includes lathe machine, Profile due to heat and flank wear combinations. Flank and crater wear on the rake face and hard metal deposition due to damages occurred during process.

J. U. Jeon and S. W. Kim works on the optical flank wear monitoring of cutting tools by image processing. The method is based on real time vision technology in which the tool is illuminated by the beam of a laser and the wear zone is visualized using a Videocon camera. The image is converted into digital pixel data and processed, to detect the wear land width. It has been proved that the average and maximum peak values of the flank wear width can be monitored effectively to a measuring resolution of 0.1

Yoram Koren, Tsu-Ren Ko, A. Galip Ulsoy, Kourosh Danai designed to operate under varying cutting conditions. For online estimation of flank wear rate based on cutting force measurements is introduced. The main aim is to employ a model of the relationship between force and flank wear, together with on-line parameter estimation method. Experiments, conducted for turning operations with a varying depth of cut, results good agreement between estimated wear values and the actual values of tool wear measured intermittently during the cut.

A mechanics of cutting analysis for orthogonal cutting with tool flank wear is presented based on an experimental investigation by J. Wang, C.Z. Huang, W.G. Song (et al. 2003). Tool flank wear results in a substantial increase in the force components and that the thrust force is more sensitive to tool flank wear. These may be used as a primary basis for developing tool condition monitoring strategies.

Tool flank wear analyses on martensitic stainless steel by turning S. Thamizhmnaii\*, B. Bin Omar, S. Saparudin, S. Hasan (et al. 2008). The flank wear was caused by abrasive action between cutting tool and work piece. The heat generated between work piece and tool tip help to form built up edge. The generated heat was conducted easily due to low thermal conductivity of the work piece material. At low cutting speed of 125 m / min with high feed rate of 0.125 mm / rev and 1.00 mm DOC.

Vishal S. Sharma, Manu Dorga, Raman Bedi, Puneet Sharma (et al. 2008) presents the experimental investigation of machining Grey Cast Iron (GCI) with uncoated carbide tools. Two models are developed for tool wear estimation, the first model is regression based and the second one is neuro-fuzzy based. They were observed that both the models are capable of predicting tool wear with good accuracy but the regression model performed marginally better than the neuro-fuzzy model.

The modelling work is not reported using tool wear area as an input parameter in prediction of tool wear. The

is used to monitor the tool wear in turning. The ultrasonic published work focus on flank wear in which input

#### II. EXPERIMENTAL DETAILS

forces. High cutting forces are identified and this may be Projector PP 200. To approach these points Mild Steel is used to study flank wear.

The experimental set up was set for the three machining diffusion of metals on the cutting tool surface are the parameters cutting speed (rpm), feed (mm/rev), and depth of cut (mm). The mild steel material chemical composition was Carbon 0.16-0.18%, Sulphur 0.040% Phosphorus 0.040% max. The following specifications are selected for this study:

Table 1: Specifications of workpiece, Cutting conditions, Profile projector and lathe machine.

Length of the workpiece Cutting Conditions Cutting Speed 32,52,88,150,250 rpm Feed 0.05,0.70,0.9,1.1,1.3 mm Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification 10x, 20x, 50x & 100x Work Stage Some 150*150 mm with X-Y movement of 25*25 mm Working Distance 270 and magnification 280 and magnification 380 mm approximately under 10x magnification 280 and magnification 380 mm approximately under 10x magnification 380 mm approxima	Work piece (Mild steel)				
workpiece Cutting Conditions Cutting Speed 32,52,88,150,250 rpm Feed 0.05,0.06,0.07,0.08,0.09 mm/rev Depth Of Cut 0.5,0.7,0.9,1.1,1.3 mm Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification 10x, 20x, 50x & 100x Work Stage Single nose or optically provided quadrapule ball bearing Working Distance 10x magnification Working Distance 2cro adjustment, 25 mm graduations with least count 0.005 mm Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W Optional 2cro adjustment & fuse 2 nos. Accessories Chylen LATHE HMT LTM20-Centre Lathe) Swing Over Bed(dia) 420 mm Distance Between Centres Spindle Drive Gear Spindle Speed 32 to 1200 rpm Spindle Socket Taper 7aper of Tails Stock Spindle Main Motor 3 K.W.					
Cutting Conditions Cutting Speed 32,52,88,150,250 rpm Feed 0.05,0.06,0.07,0.08,0.09 mm/rev Depth Of Cut 0.5,0.7,0.9,1.1,1.3 mm Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification 10x, 20x, 50x & 100x Work Stage Solution 10x magnification Working Distance 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Counter LATHE HMT LTM20-Centre Lathe) Swing Over Bed(dia) 420 mm Distance Between Centres Spindle Drive Gear Spindle Socket Taper Taper of Tails Stock Spindle Main Motor 3 K.W.		60 mm			
Cutting Speed 32,52,88,150,250 rpm Feed 0.05,0.06,0.07,0.08,0.09 mm/rev Depth Of Cut 0.5,0.7,0.9,1.1,1.3 mm Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification 10x, 20x, 50x & 100x 150*150 mm with X-Y movement of 25*25 mm  Work Stage 30 mm approximately under 10x magnification Zero adjustment, 25 mm graduations with least count 0.005 mm Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover, duster & fuse 2 nos.  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe) Swing Over Bed(dia) 420 mm Distance Between Centres Spindle Drive Gear Spindle Speed 32 to 1200 rpm Spindle Speed MT 4  Travel of Tails Stock Spindle Main Motor 3 K.W.		l			
Feed 0.05,0.06,0.07,0.08,0.09 mm/rev Depth Of Cut 0.5,0.7,0.9,1.1,1.3 mm  Profile Projector(PP-200)  Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable  Single nose or optically provided quadrapule ball bearing  Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 2cro adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover , duster & fuse 2 nos.  Accessories Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper Taper of Tails Stock Spindle  Main Motor 3 K.W.		32.52.88.150.250 rpm			
Depth Of Cut Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification Work Stage Working Distance  Micrometer  Micrometer  Single nose or optically provided quadrapule ball bearing Tox, 20x, 50x & 100x  150*150 mm with X-Y movement of 25*25 mm  30 mm approximately under 10x magnification Zero adjustment, 25 mm graduations with least count 0.005 mm Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe) Swing Over Bed(dia) Distance Between Centres Spindle Drive Spindle Speed Spindle Speed Spindle Socket Taper Travel of Tails Stock Spindle Main Motor  3 K.W.		0.05.0.06.0.07.0.08.0.09 mm/rev			
Profile Projector(PP-200) Focussing Through rack and pinion system Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable Single nose or optically provided quadrapule ball bearing Magnification 10x, 20x, 50x & 100x 150*150 mm with X-Y movement of 25*25 mm  Working Distance Micrometer  Working Distance Zero adjustment, 25 mm graduations with least count 0.005 mm Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe) Swing Over Bed(dia) Distance Between Centres Spindle Drive Spindle Speed 32 to 1200 rpm Spindle Socket Taper Taper of Tails Stock Spindle Main Motor 3 K.W.					
Focussing  Through rack and pinion system  Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable  Single nose or optically provided quadrapule ball bearing  Magnification  Tox, 20x, 50x & 100x  150*150 mm with X-Y movement of 25*25 mm  Working Distance  Working Distance  Micrometer  Tox magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Speed  Spindle Speed  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Spindle  Main Motor  3 K.W.					
Screen  Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable  Single nose or optically provided quadrapule ball bearing  Magnification  10x, 20x, 50x & 100x  150*150 mm with X-Y movement of 25*25 mm  Working Distance  Micrometer  Micrometer  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Speed  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock  Spindle  Main Motor  Antiglare hard glass 200 mm diameter with cross line, 360 degree rotatable  Single nose or optically provided quadrapule ball bearing  Single nose or optically provided quadrapule ball bearing  Spindle Socket Taper  60 metric  Taper of Tails Stock  Spindle  Main Motor  3 K.W.					
Screen diameter with cross line, 360 degree rotatable  Single nose or optically provided quadrapule ball bearing  Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 20m approximately under 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover , duster & fuse 2 nos.  Accessories Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve Travel of Tails Stock Spindle  Main Motor 3 K.W.					
Nosepiece Single nose or optically provided quadrapule ball bearing  Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 30 mm approximately under 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover, duster & fuse 2 nos.  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve 150 mm  Main Motor 3 K.W.	Screen				
Nosepiece provided quadrapule ball bearing  Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 30 mm approximately under 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover , duster & fuse 2 nos.  Accessories Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve 150 mm  Main Motor 3 K.W.		degree rotatable			
Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 30 mm approximately under 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover , duster & fuse 2 nos.  Accessories Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve 150 mm  Main Motor 3 K.W.		Single nose or optically			
Magnification 10x, 20x, 50x & 100x  Work Stage 150*150 mm with X-Y movement of 25*25 mm  Working Distance 30 mm approximately under 10x magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover, duster & fuse 2 nos.  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.	Nosepiece				
Work Stage    150*150 mm with X-Y movement of 25*25 mm	•	bearing			
Working Distance  Working Distance  Micrometer  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Vinyl cover , duster & fuse 2 nos.  Accessories  Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Speed  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  3 K.W.	Magnification	10x, 20x, 50x & 100x			
Working Distance    30 mm approximately under 10x magnification     Zero adjustment, 25 mm graduations with least count 0.005 mm     Counter illuminator of 12V-100W & 2 Surface lamps of 6V/20W     Optional   Vinyl cover , duster & fuse 2 nos.     Accessories   Objective 40x , 80x , Halogen Bulb, Digital Micrometers     Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)     Swing Over Bed(dia)   420 mm     Distance Between Centres   1000 mm     Spindle Drive   Gear   Spindle Speed   32 to 1200 rpm     Spindle Socket Taper   60 metric     Taper of Tails Stock   Sleeve     Travel of Tails Stock   Spindle     Main Motor   3 K.W.	Waste Ctara	150*150 mm with X-Y			
Micrometer  Micrometer  Micrometer  Micrometer  Micrometer  Description:  Micrometer  Micrometer  Micrometer  Description:  Micrometer  Micrometer  Micrometer  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Vinyl cover , duster & fuse 2 nos.  Accessories  Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Jox magnification  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Vinyl cover , duster & fuse 2 nos.  Accessories  Distance Betwee 1 1000 mm  Gear Spindle Speed  32 to 1200 rpm  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  3 K.W.	work Stage	movement of 25*25 mm			
Micrometer  Zero adjustment, 25 mm graduations with least count 0.005 mm  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Journal Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Vinyl cover, duster & fuse 2 nos.  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  1000 mm  Gear 1000 mm  For in the property of the propert	Wl-i Di-t	30 mm approximately under			
Micrometer graduations with least count 0.005 mm  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover, duster & fuse 2 nos.  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres Spindle Drive Gear Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle Main Motor 3 K.W.	working Distance	10x magnification			
Illumination  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Over Illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Vinyl cover, duster & fuse 2 nos.  Accessories  Pobjective 40x, 80x, Halogen Bulb, Digital Micrometers  420 mm  1000 mm  Gear Spindle Drive Gear Spindle Socket Taper Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle Main Motor  3 K.W.					
Illumination  Counter illuminator of 12V- 100W & 2 Surface lamps of 6V/20W  Optional  Vinyl cover , duster & fuse 2 nos.  Objective 40x , 80x , Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Accessories  Vinyl cover , duster & fuse 2 nos.  Objective 40x , 80x , Halogen Bulb, Digital Micrometers  1000 mm  60 mm  60 metric  MT 4  150 mm  Main Motor  3 K.W.	Micrometer	graduations with least count			
Illumination 100W & 2 Surface lamps of 6V/20W  Optional Vinyl cover, duster & fuse 2 nos.  Accessories Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.					
Optional  Optional  Vinyl cover, duster & fuse 2 nos.  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Drive  Gear  Spindle Speed  32 to 1200 rpm  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  3 K.W.					
Optional  Vinyl cover, duster & fuse 2 nos.  Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Vinyl cover, duster & fuse 2 nos.  Halogen Bulb, Digital Micrometers  420 mm  1000 mm  Gear  50 metric  MT 4  150 mm  Main Motor  3 K.W.	Illumination	100W & 2 Surface lamps of			
Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Gear Spindle Speed  Spindle Socket Taper Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  1000 mm  1000 mm  60 metric  MT 4					
Accessories  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia)  Distance Between Centres  Spindle Drive  Spindle Speed  Spindle Socket Taper  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  Objective 40x, 80x, Halogen Bulb, Digital Micrometers  420 mm  1000 mm  Gear  Spindle Speed  32 to 1200 rpm  MT 4  Taper of Tails Stock Sleeve  Travel of Tails Stock Spindle  Main Motor  3 K.W.	Ontional	Vinyl cover, duster & fuse 2			
Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres 1000 mm  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.	Ориони	nos.			
Lathe Machine(CENTRE LATHE HMT LTM20-Centre Lathe)  Swing Over Bed(dia) 420 mm  Distance Between Centres  Spindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.	A accessories	Objective 40x, 80x, Halogen			
Lathe)  Swing Over Bed(dia) 420 mm  Distance Between 1000 mm  Centres 5pindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.	Accessories				
Lathe)  Swing Over Bed(dia) 420 mm  Distance Between 1000 mm  Centres 5pindle Drive Gear  Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle  Main Motor 3 K.W.	Lathe Machine(CENTRE	ELATHE HMT LTM20-Centre			
Distance Between Centres  Spindle Drive Gear Spindle Speed Spindle Socket Taper Taper of Tails Stock Sleeve Travel of Tails Stock Spindle Main Motor  1000 mm  Gear 32 to 1200 rpm 60 metric MT 4  150 mm					
Distance Between Centres  Spindle Drive Gear Spindle Speed Spindle Socket Taper Taper of Tails Stock Sleeve Travel of Tails Stock Spindle Main Motor  1000 mm  Gear 32 to 1200 rpm 60 metric MT 4  150 mm	Swing Over Bed(dia)	420 mm			
Spindle Drive Gear Spindle Speed 32 to 1200 rpm Spindle Socket Taper 60 metric Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle Main Motor 3 K.W.		1000			
Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle 150 mm  Main Motor 3 K.W.	Centres	1000 mm			
Spindle Speed 32 to 1200 rpm  Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle 150 mm  Main Motor 3 K.W.	Spindle Drive	Gear			
Spindle Socket Taper 60 metric  Taper of Tails Stock Sleeve MT 4  Travel of Tails Stock Spindle 150 mm  Main Motor 3 K.W.					
Taper of Tails Stock Sleeve Travel of Tails Stock Spindle Main Motor  Taper of Tails Stock Sleeve 150 mm 3 K.W.					
Sleeve M1 4  Travel of Tails Stock Spindle 150 mm  Main Motor 3 K.W.		MT 4			
Spindle 150 mm  Main Motor 3 K.W.					
Main Motor 3 K.W.	Travel of Tails Stock	150 mm			
		130 11111			
Net Weight 1250 kg					
	Net Weight	1250 kg			



ISO 3297:2007 Certified Vol. 3, Issue 7, July 2016



Fig: Lathe Machine (CENTRE LATHE HMT LTM20-Centre Lathe)`

#### **III.REGRESSION**

Since multiple regression is used to determine a correlation between a criterion variable and a combination of predictor variables, the statistical multiple regression method is applied. It can be used to analyze the data from any of the major quantitative research designs such as causal-comparative, correctional and experimental.

This method is able to handle interval, ordinal, or categorical data and provide estimates both of the magnitude and statistical significance of the relationships between variables Therefore, multiple regression analysis will be able to predict the criterion variable finish surface roughness via predictor variables such as feed rate, spindle speed, depth of cut and work piece material hardness (M. S. Lou et al. 1998).

After experimentation on tool material 125 datasets are collected. Out of this data set 100 data sets are used for training and randomly selected 25 data sets (1/4<sup>th</sup> of total data sets) for testing prediction accuracy. An empirical expression was established based on the regression analysis for predicting wear of dry turning.

 $VB = 0.0114465 \, S^{(0.013)} F^{(-1.114)} D^{(0.803)}$ 

Where, VB- Flank Wear (mm),

S-cutting speed in RPM, F-feed in mm/rev, D-depth of cut in mm.

The above new empirical model is developed for prediction of flank wear using speed, feed, and depth of cut. It is also observed that the proposed equation establishes the relation among input variables and prediction model.

### IV.ADAPTIVE NEURO-FUZZY INFERENCE SYSTEM (ANFIS)

Although the fuzzy inference system has a structured knowledge representation in the form of a fuzzy "if-then" rule, it lacks the adaptability to deal with changing external environment. Therefore neural network learning concepts have been incorporated in a fuzzy inference system, resulting in adaptive neuro-fuzzy modelling. Adaptive inference system is a network that consists of a number of interconnected nodes.

Each node is characterized by a node function with fixed or adjustable parameter. The network is "learning" the behaviour of the available data during a training phase by adjusting the parameters of the node functions to fit the data. The basic learning an algorithm, the back propagation, aims on the minimization of a set measure or a defined error, usually the sum of the squared differences between the desired and the actual model outputs.

ANFIS is a famous hybrid neuro-fuzzy network for modelling complex systems and was developed by Jang (1993). This system is a useful neural network approach for the solution of a nonlinear functions and approximating problems (2008). The system refers to the way of applying various learning techniques are developed in the literature to a fuzzy inference system (FIS). Fig. shows the basic structure of a FIS that consists of a five functional blocks: a rule base, which contains a number of fuzzy if-then rules; a database, which defines a membership functions (MF) of the fuzzy sets; a decisionmaking unit as the inference engine, a fuzzification interface, which transforms the crisp inputs to linguistic variables; and a defuzzification interface, which converts the fuzzy outputs to crisp outputs.

The proposed neuro-fuzzy model of the ANFIS is a multilayer neural network-based fuzzy system. Both the neural network (NN) and fuzzy logic (FL) are used in ANFIS architecture. The system has an adaptive network which is functionally equivalent to a 1st-order Sugeno fuzzy inference system Jang (1993). The ANFIS uses a hybrid-learning rule, which combines back-propagation, gradient-descent and least squares algorithm to identify and optimise the Sugeno system's signals and a corresponding equivalent ANFIS architecture of a firstorder Sugeno fuzzy model with two rules? The square nodes are the adaptive nodes, and the circular nodes are fixed nodes whose parameters change during the training process.

The system has the total of five layers. In this connected structure, the input and output nodes represents the training and a predicted values, respectively, and in the hidden layers, there are nodes functioning as the response variables. The average deviation observed in membership functions (MFs) and rules. This architecture measured value 28.47% at confidence level of 85%. This has a benefit that it eliminates the disadvantage of a regression prediction values are used for comparison with normal feed forward multilayer network, where it is a ANFIS prediction model values to verify the accuracy of a difficult for an observer to understand or modify the network.



ISO 3297:2007 Certified Vol. 3, Issue 7, July 2016

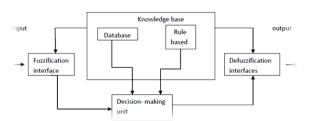


Figure 3: Block diagram of ANFIS (Jang 2004)

#### V. RESULTS AND DISCUSSION

The experimental data 125 set was collected out of which 100 datasets were utilized as a training data and remaining 25 data sets as a testing data. The fuzzy inference system was trained up to 100 epochs. To verify the accuracy of prediction other 25 sets were used as a testing data. In this experiment ANFIS triangular MF, VB is compared regression analysis VB value. Therefore the prediction accuracy of ANFIS triangular MF is higher as compare to regression prediction models. It is also observed that predicted flank wear accuracy is 87.87% with triangular membership function with average deviation of a 12.13%. Where as in regression analysis the average deviation observed is 28.47%. Flank Wear in Turning (Dry) Testing Data:

Table 2: Experimental, Predicted flank wear and percentage error
Flank wear Prediction using ANFIS using Trapezoidal Membership Function

Sr.	Spee	Fee	De	Flank	ANF	% Error
no.	d(rp	d(m	pth	wear	IS	
	m)	m/re	of	Exper	Trap	
		v)	cut	iment	MF	
			(m			
			m)			
1	32	0.05	1.3	0.45	0.429	4.67
2	52	0.05	1.1	0.45	0.491	9.11
3	88	0.05	1.3	0.4	0.439	9.75
4	150	0.05	1.1	0.45	0.423	6
5	250	0.05	1.3	0.28	0.502	79.29
6	32	0.06	1.1	0.25	0.212	15.2
7	52	0.06	1.3	0.23	0.255	10.87
8	88	0.06	1.1	0.22	0.216	1.82
9	150	0.06	1.3	0.23	0.271	17.83
10	250	0.06	0.7	0.11	0.139	26.36
11	32	0.07	1.3	0.23	0.255	10.87
12	52	0.07	1.3	0.22	0.255	15.91
13	88	0.07	0.5	0.11	0.097	12.27
14	150	0.07	0.9	0.17	0.166	2.35
15	250	0.07	1.3	0.29	0.249	14.14
16	32	0.08	1.1	0.21	0.228	8.57
17	52	0.08	1.3	0.41	0.283	30.98
18	88	0.08	0.9	0.185	0.18	2.7
19	150	0.08	1.3	0.31	0.297	4.19
20	250	0.08	0.5	0.117	0.111	5.13

21	32	0.09	1.3	0.32	0.308	3.75		
22	52	0.09	0.5	0.12	0.114	5		
23	88	0.09	0.9	0.195	0.191	2.05		
24	150	0.09	1.3	0.325	0.321	1.23		
25	250	0.09	0.5	0.125	0.121	3.2		
	Average Error 12.13							

#### VI. CONCLUSIONS

An ANFIS is used to measure flank wear the turning parameters Cutting speed, Feed and Depth of Cut in turning process. Out of 125 data sets 25 sets of data are used as testing data. The measured values of flank wear are compared with ANFIS predicted values. Within the ANFIS triangular membership function is used for prediction of tool wear. The flank wear prediction accuracy by ANFIS with triangular membership function is 87.87% with the error of 12.13%. The ANFIS with triangular membership function also outperforms the regression analysis model in terms of prediction accuracy. ANFIS prediction model using trapezoidal membership function are observed better with speed, feed, depth of cut as input parameters in flank wear prediction. Flank wear with regression average error is 28.47% which is not suitable for any prediction. But when this experiment is done with ANFIS then it is observed that ANFIS is more suitable for the prediction of tool wear.

#### REFERENCES

- Mr. R. Srinidhi, Dr. Vishal Sharma, Dr. M.Sukumar, Dr. C. S. Venkatesha "Correlative flank wear analysis of single point turning inserts using acostic emission and artificial intelligence techniques"
- Heyao Shen, Minghong Wang. "The simulation analysis of tool flank wear based on cutting force" ISSN: 2319-1163
- D. Dinakaran, S. Sampathkumar, J. Susai Mary (2010) "Real time prediction of flank wear by nuero fuzzy technique in turning." JJMIE ISSN 1995-6665.
- S. Thamizhmanii\*, S. Hasan 2008. "Measurement of surface roughness and flank wear on hard martensitic stainless steel by CBN and PCBN cutting tools"
- J. U. Jeon and S. W. Kim(1988)" Optical flank wear monitoring of cutting tools by image processing"
- Yoram Koren, Tsu-Ren Ko, A. Galip Ulsoy, Kourosh Danai " Flank wear under varying cutting conditions."
- J. Wang, C.Z. Huang1, W.G. Song "The effects of tool flank wear on the orthogonal cutting process and its practical implications." Journal of Materials Processing Technology 142 (2003) 338–346.
- S.Thamizhmanii\* and S.Hasan "Relationship between Flank wear and Cutting Force on the Machining of Hard Martensitic Stainless Steel by Super Hard Tools" Proceedings of the World Congress on Engineering 2010.
- Vishal S. Sharma, Manu Dorga, Raman Bedi, Puneet Sharma (2008) "Regression versus neuro-fuzzy model: A comparison for tool wear estimation".
- Lou, M. S., Chen, J. C., & Li, C. M. (1998). "Surface roughness technique for CNC End milling". Journal of Industrial Technology, 15 (1), 1-6.
- J.S.R. Jang, "ANFIS: adaptive-network-based fuzzy inference system", IEEE Transactions on System, Man, and Cybernetics 2 (3) (1993) 665–685.
- Purushottam S. Desale and Ramchandra S. Jahagirdar.,2013, "Modeling the effect of variable work piece hardness on surface roughness in an end milling using multiple regression and adaptive Neuro fuzzy inference system", International Journal of Industrial Engineering Computations 5 (2014) 265–272.